

# Comparison of IPD and Fuzzy Logic Velocity Control In Two Degree of Freedom DC Motor System

Adem AVCU\*, Ahmet F. BOZKURT\*\*, Kadir ERKAN\*\*, Semih SEZER\*, İlkey KURT\*

\*Mechanical Engineering, Faculty of Mechanical Engineering, Yıldız Technical University, 34349, Turkey

\*\*Mechatronics Engineering, Faculty of Mechanical Engineering, Yıldız Technical University, 34349, Turkey

(ademavcu01@gmail.com,afbozkurt90@gmail.com,kerkan@yildiz.edu.tr,sezer@yildiz.edu.tr, ikurt@yildiz.edu.tr)

‡Corresponding Author; AdemAvcu, Yıldız Technical University, Istanbul, TURKEY, Tel: +90 212 383 2776 Fax: +90 212 383 3025, ademavcu01@gmail.com

*Received: 19.01.2018 Accepted: 02.03.2018*

**Abstract-** In this study, IPD and Fuzzy Logic Controller (FLC) are applied separately to perform velocity control of the system that has two degree of freedom in real time. IPD controller uses coefficients which are integral, differential and proportional are calculated with Coefficient Diagram Method (CDM). This method is based on polynomial approach and has many advantages such as easy design procedure, an interpretation of settling time, stability and parameter tuning. FLC uses linguistic variables and can be applied easily. IPD and FLC results are compared in terms of current, voltage and velocity for reference input.

**Keywords** IPD, FLC, CDM, velocity control, reference input.

## 1. Introduction

DC motors are widely used industrial areas because of the advantages and convert electrical energy into rotational mechanical energy. DC motors have relatively low cost to the other motor types, such as servo, step, brushless DC etc., facility of control with uncomplicated motor drive circuits and can produce high torque in the first operation, operate under heavy loads and reverse direction operation can be done by changing the polarity of the poles.

PID controller is usually used in industrial environments and devices because of its simplicity. PID control design is based on mathematical model so it requires system transfer function. PID means proportional, integral, differential control coefficients and it can be described as controller transfer function. Generally, Ziegler-Nichols method is used to calculate the coefficients of PID. On the contrary, regular PID controller structures can be more efficient by changing structures of IPD in order to have less overshoot. IPD controller is usually used in precise control applications [1 2].

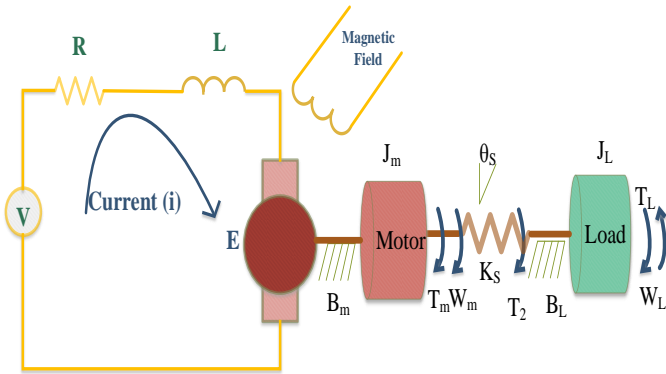
The Coefficients of IPD controller which are integral, differential and proportional can be calculated easily and effectively with using Coefficient Diagram Method (CDM). It is suggested from Shunji Manabe in 1991, since that date it has begun to be used in different control applications. It gives possibilities which are resistance to inner and outer disturbances, lower overshoot of system answer, easy design and implementation, for simple and complex systems [3-5].

Fuzzy Logic Controller was suggested as a new type of controller by A. Zadeh in 1964. It uses not only 1 and 0 but besides them; numbers between 1 and 0 are used, so FLC gives robust control facility. There are many advantages to use FLC. For example, no mathematical equations, capability of using linguistic and numerical variables, possibility of application in all fields [5]. Apart from the PID controller structure, PI, PD, PIDP or IPD structures can be used. By comparing these control structures with FLC, it can be decided which one is a better choice for desired conditions. Moreover, a controller can be designed with combinations of FLC and PID or IPD controller [6-10].

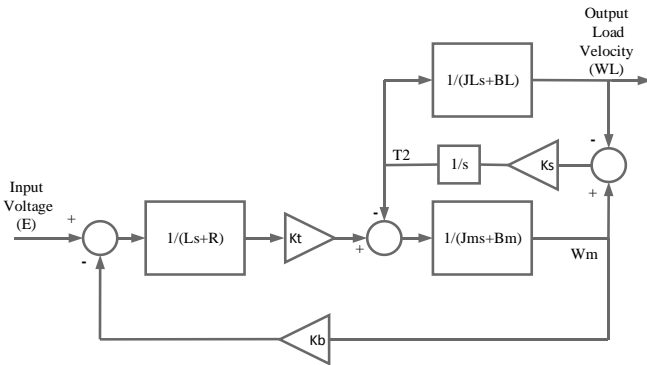
In two degree of freedom, systems have two mass or two rotary inertia. One of the motor is source of movement and the other inertia is the load. Strap or coupling machine elements can be used to transfer motion from one to the other [11 12]. In this study, the system consists of two DC motors with different inertia pulleys and one of DC motor is chosen as driver and the other one as load. Flexible strap is used for transfer motion and behaves like a spring. Coefficients of IPD controller are calculated with using Coefficient Diagram Method which is polynomial approach. IPD and FLC are applied to experiment system separately then the results are compared.

**2. Mathematical Model of The System**

DC motor system converts electrical energy to mechanical energy then motion is transferred to the load inertia by elastic belt. The system is shown physical in Fig.1 and block diagram schema in Fig.2



**Fig. 1.** The system schema



**Fig. 2.** The system block diagram

**Table 1.** System Variables

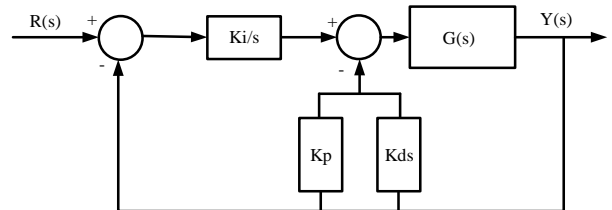
Symbol	Definitions	Units
$K_b$	Electromotive Force	V.s/Rad
$K_t$	Motor torque constant	N.m/A
$B_m$	Motor friction	N.m.s/rad
$R$	Armature resistance	Ohm( $\Omega$ )
$L$	Inductance of armature	Henry (H)
$J_m$	Motor inertia	Kg.m <sup>2</sup>
$E$	Back EMF	Volts (V)
$J_L$	Load inertia	Kg.m <sup>2</sup>
$i$	Armature current	Current (A)
$\theta_s$	Angular position	Radians
$W_m$	Motor Angular speed	Rad/s
$W_L$	Load Angular speed	Rad/s
$B_L$	Load friction	N.m.s/rad
$K_S$	Flexible strap	N.m/rad
$T_m$	Motor torque	N.m
$T_L$	Load torque	N.m
$T_2$	Strap torque	N.m
$V$	Input voltage	Volts (V)

Transfer function of system is given in Eq. (1) with respect to input voltage (V) and load angular velocity ( $W_L$ ).

$$\frac{W_L(s)}{V(s)} = \frac{K_t \cdot K_s}{((J_m s + B_m) \cdot (Ls + R) + K_t \cdot K_b) \cdot (J_L s^2 + B_L s + K_s)} \quad (1)$$

**3. Designing of IPD Controller**

The IPD controller ensures more stability with using CDM which gives the coefficients of IPD. The IPD controller structure is given in Fig.3. Expression of letter are reference input R(s), output Y(s) and transfer function of system G(s).



**Fig. 3.** IPD Controller structure

Substituting IPD to Eq. (1), closed loop transfer function of system with controller are obtained and given Eq. (2)

$$TF = \frac{K_i K_s K_t}{A+B+C} \quad (2)$$

Where;

$$A = J_m J_L L s^5 + J_m J_L R s^4$$

$$B = (J_m L K_s + J_L K_b K_t) s^3 + (J_m R K_s + K_d K_s K_t) s^2$$

$$C = (K_p K_s K_t + K_b K_s K_t) s + K_i K_s K_t$$

Characteristic polynomial is obtained from Eq. (2)

$$KP = A + B + C \quad (3)$$

Characteristic polynomial coefficient is used with Manabe Form which is given in Table 2.

**Table 2.** Standart Manabe Form

	<i>n</i>	<i>Y<sub>i</sub></i>	<i>Y<sub>i+1</sub></i>	<i>Y<sub>i+2</sub></i>	<i>Y<sub>i+3</sub></i>	<i>Y<sub>i+4</sub></i>
<b>Manabe Form</b>	4	2.5	2	2		
	5	2.5	2	2	2	
	6	2.5	2	2	2	2

By using Manabe form and characteristic polynomial, time constant ( $\tau$ ), index ( $\gamma_1, \gamma_2$ ) equations are obtained and given below.

$$\tau = \frac{a_1}{a_0}; \tau = \frac{(K_p K_s K_t + K_b K_s K_t)}{K_i K_s K_t} \quad (5)$$

$$\gamma_1 = \frac{a_1^2}{a_2 \cdot a_0}; \gamma_1 = \frac{(K_p K_s K_t + K_b K_s K_t)^2}{(J_m R K_s + K_d K_s K_t) \cdot (K_i K_s K_t)} \quad (6)$$

$$\gamma_2 = \frac{a_2^2}{a_3 \cdot a_1}; \gamma_2 = \frac{(J_m R K_s + K_d K_s K_t)^2}{(J_m L K_s + J_L K_b K_t) \cdot (K_p K_s K_t + K_b K_s K_t)} \quad (7)$$

Solving Eq. (5, 6, 7),  $K_i, K_p$  and  $K_d$  coefficients are calculated and given in Eq. (8, 9, 10).

$$K_i = \frac{(J_m \cdot L \cdot \gamma_1^2 \cdot \gamma_2 \cdot K_s + J_L \cdot \gamma_1^2 \cdot \gamma_2 \cdot K_b \cdot K_t)}{(\tau^3 \cdot K_s \cdot K_t)} \quad (8)$$

$$K_p = \frac{(J_m \cdot L \cdot \gamma_1^2 \cdot \gamma_2 \cdot K_s - \tau^2 \cdot K_b \cdot K_s \cdot K_t + J_L \cdot \gamma_1^2 \cdot \gamma_2 \cdot K_b \cdot K_t)}{(\tau^2 \cdot K_s \cdot K_t)} \quad (9)$$

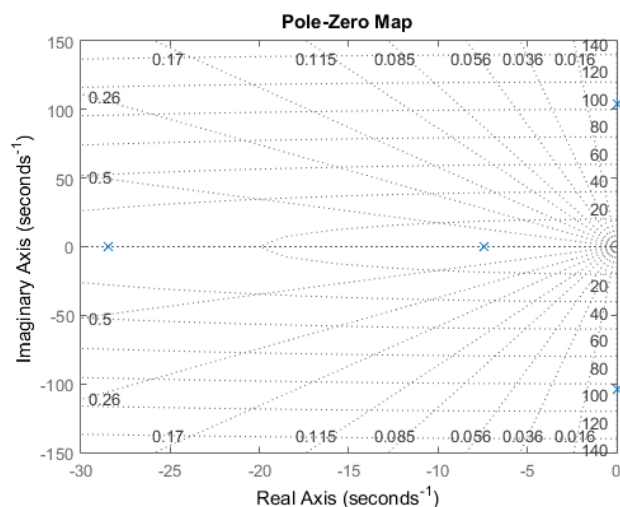
$$K_d = - \frac{(J_m \cdot L \cdot \gamma_1^2 \cdot \gamma_2 \cdot K_s - J_m \cdot R \cdot \gamma_1 \cdot \gamma_2 \cdot K_s + J_L \cdot \gamma_1^2 \cdot \gamma_2 \cdot K_b \cdot K_t)}{(\tau \cdot \gamma_1 \cdot K_s \cdot K_t)} \quad (10)$$

Control system parameters can be obtain by using Manabe Form; time constant and index where;  $\tau=0.12, \gamma_1=2.5, \gamma_2=2$ . System characteristic values are given in Table 3. Afterwards, substituting values in Eq. (8, 9, 10) coefficients are obtained as  $K_i=5.4, K_p=0.5, K_d=-0.0048$ .

**Table 3.** System characteristic values

Motor	Value	Unit
$K_b$	0,155	Vs/Rad
$K_t$	0,137	Nm/A
$B_m$	0,00095	Nm/rad/sec
R	3,592	Ohm
L	0.1	Henry
$J_m$	0.001	Kgm <sup>2</sup>
<b>Load</b>		
$J_L$	0.0001	Kgm <sup>2</sup>
$B_L$	0,00086	Nm/rad/sec
<b>Flexible Strap</b>		
$K_s$	1.09	Nm/rad

The system's open loop roots are shown in Fig. 4. When the roots are examined, it seems that they are marginally stable. In addition, the closed loop root placement graphics determined by the Coefficient Diagram Method, IPD controller is shown in Fig.5, and the marginally stable roots are replaced as stable roots.



**Fig. 4.** The roots of open loop

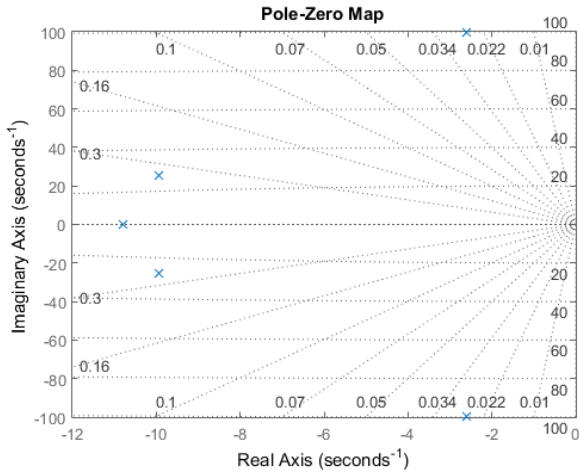


Fig. 5. The roots of closed loop

4. Designing of Fuzzy Logic Controller

The fuzzy logic controller is designed by analyzing the behavior of the system without mathematical model subsequently, based on knowledge as If-Then rules. FLC If-Then statements are associated by membership functions are prepared for inputs and outputs. The more membership functions are defined, the more successful of control of system becomes possible, and so controller system rules are designed as 7x7. The Linguistic variables defining the rule base for the fuzzy logic controller are given in Table 4. Membership ranges are named NB, NM, NS, Z, PB, PM, PS represent “Negative big”, “Negative medium”, ”Negative small”, ” Zero”, “Positive big”, “Positive medium”, “Positive small”, respectively.

The fuzzy logic control is achieved fuzzification operation and output value is determined by FLC decision operation after the specified rules. FLC uses Linguistic variable instead of numerical variable. The numerical variables are converted to linguistic variables, which is named fuzzification. FLC inference engine decide output with using Fuzzy rules. Linguistic variables give output in numerical by defuzzification operation. This condition is stated in Fig.6. In Fuzzy Logic Controller structure, error and error change are applied to FLC as input, thereafter; it gives voltage to the system as output. The designed FLC is given in Fig.7.

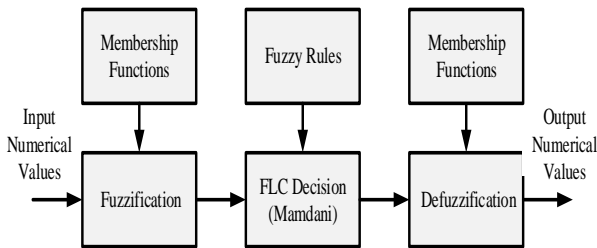


Fig. 6. Fuzzy Logic Controller structure

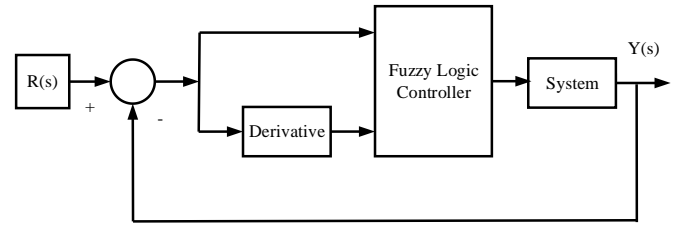


Fig. 7. Application Form FLC to system

Velocity error, derivative of velocity error and output membership functions are given respectively in Figures (8-9-10). Surface graph generated by input and output membership functions is shown in Fig.11. Velocity error and derivative of velocity error rules are matched to output rules, which are given in Table 4.

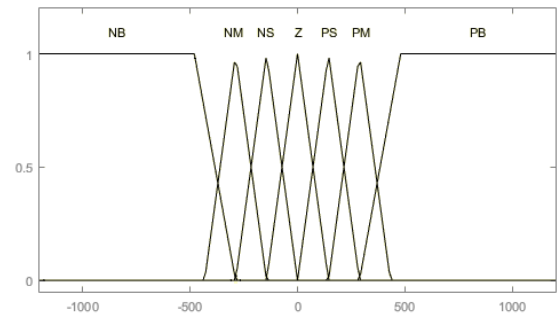


Fig. 8. Velocity Error Membership Functions

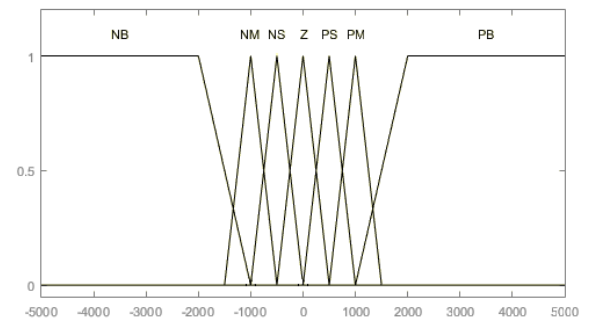


Fig. 9. Derivative of Velocity Error Membership Functions

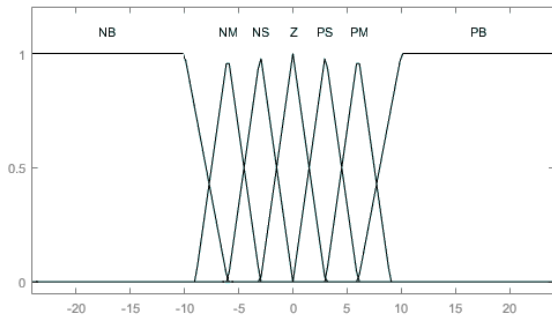


Fig. 10. Output Membership Functions

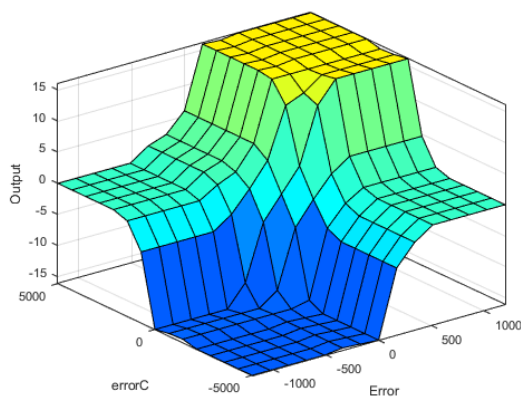


Fig. 11. FLC Surface

Table 4. The system Fuzzy Logic Controller rules table

	<i>Derivative of Velocity Error</i>						
<i>Velocity Error</i>	<i>NB</i>	<i>NM</i>	<i>NS</i>	<i>Z</i>	<i>PS</i>	<i>PM</i>	<i>PB</i>
<i>NB</i>	NB	NB	NB	NB	NM	NS	Z
<i>NM</i>	NB	NB	NB	NM	NS	Z	PS
<i>NS</i>	NB	NB	NM	NS	Z	PS	PS
<i>Z</i>	NB	NM	NS	Z	PS	PM	PM
<i>PS</i>	NM	NS	Z	PS	PS	PB	PB
<i>PM</i>	NS	Z	PS	PM	PM	PB	PB
<i>PB</i>	Z	PS	PM	PB	PB	PB	PB

### 5. The Experimental System

The The system is designed with two DC motor, 100w DC motor acts as the driver motor and 140w DC motor is used as the load. Flexible strap is used to transfer motion from driver to the load. DC motor velocity information is gained from 140w load motor by attached 360p encoder. To control system, Quanser Q8 data acquisition card

(DAQ) is used for sending analog signals and getting encoder signals.

The system is designed by using block diagrams with Matlab-Simulink that also provides communication between computer and DAQ card. When control signal arrived to DAQ card then it sends interpretation of analog signals to H-Bridge Motor driver. In addition, to gain velocity of the load, feedback signal from 360p encoder is used. In other words, DC motor is energized from H-Bridge driver and feedback velocity information is gained from the load encoder. Flexible strap is transferred motion from motor to load. It provides flexible motion and this point differ from other two degree of freedom systems. The goal of this study, if belt stretches under inner or outer disturbances, controller should compensate the affect.

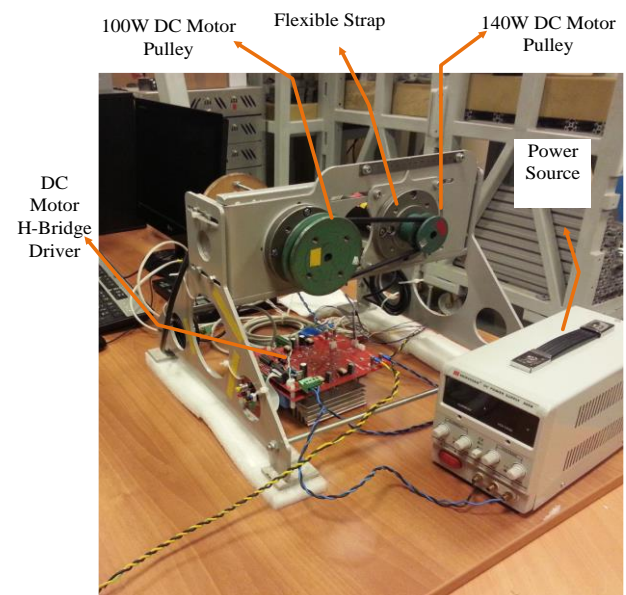


Fig. 12. Experimental System Frontside

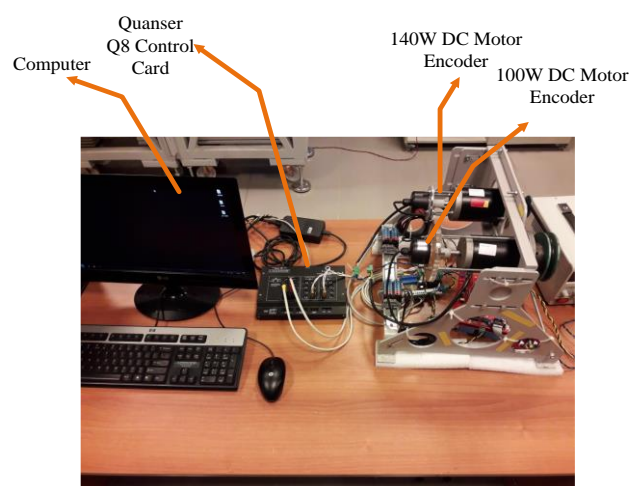


Fig. 13. Experimental System Backside

The results of CDM IPD controller and Fuzzy Logic Controller are compared in terms of current, voltage and velocity for 50 rad/s velocity input value. According to the measurement results, FLC draws more current and voltage than IPD when reference is applied, shown Fig.14 and Fig.15 respectively. When the results are examined, it is clear that FLC achieves to desired values faster than IPD controller (Fig.16). Moreover, in all three graphs, controller responses are shown according to the disturbance torque, applied between fifth and seventh second. It has been observed that FLC responds faster than IPD controller.

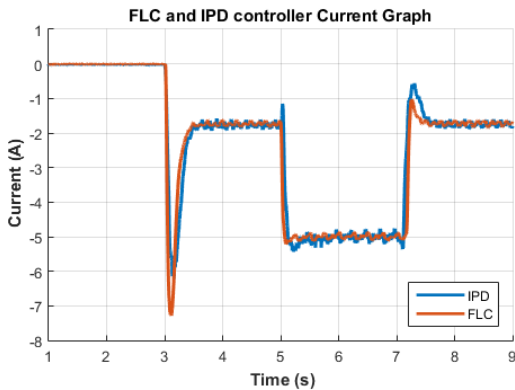


Fig. 14. IPD and FLC current graph in system velocity control

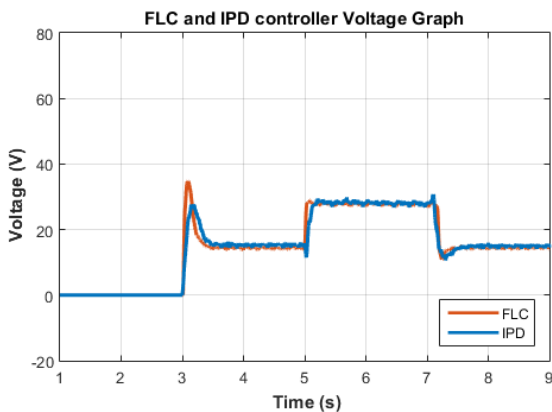


Fig. 15. IPD and FLC volt graph in system velocity control

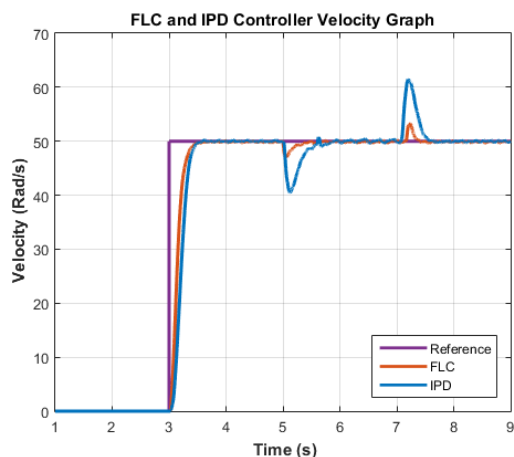


Fig. 16. IPD and FLC graph in system velocity control

## 6. Conclusion

The Two degree of freedom DC motor system is used in the study. The system transfers motor motion to load by elastic strap. Firstly, mathematical model and transfer functions of the system are obtained. Then, IPD and FLC based active control algorithm are applied to the system experimentally. CDM based IPD controller and FLC are applied for velocity control, then results of controllers are compared. FLC acts faster than IPD controller and performs better even at reference input or against output disturbance.

## Acknowledgements

Thanks to Yıldız Technical University Mechatronics Engineering Department for laboratory facilities.

## References

- [1] D. Puangdownreong, A. Nawikavatan, C. Thammarat, "Optimal Design of I-PD Controller for DC Motor Speed Control System by Cuckoo Search" ,2016 International Electrical Engineering Congress, iEECON2016, 2-4 March 2016, Chiang Mai, Thailand
- [2] Kadir Erkan, Barış Can Yalçın & Muhammet Garip, "Three-axis gap clearance I-PD controller design based on coefficient diagram method for 4-pole hybrid electromagnet", *Automatika*, 58:2, 147-167, 2017, Istanbul, Turkey
- [3] Manabe, S., "Coefficient Diagram Method" , IFAC Automatic control in Aerospace, Seoul, Korea, 1998
- [4] B. Meenakshipriya. K. Kalpana., "Modelling and Control of Ball and Beam System using Coefficient Diagram Method (CDM) based PID controller" ,Third International Conference on Advances in Control and Optimization of Dynamical Systems March 13-15, 2014. Kanpur, India
- [5] Serdar Ethem HAMAMCI, "İntegratörlü sistemler için Katsayı Diyagram Metodu ile kontrolör tasarımı" , *itüdergisi/d Mühendislik Cilt:3, Sayı:6, 3-12 Aralık 2004*
- [6] Fatih Köseç, Kaplan Kaplan, H. Metin Ertunç, "PID ve Bulanık Mantık ile DC Motorun Gerçek Zamanda STM32F407 Tabanlı Hız Kontrolü" , *Otomatik Kontrol Ulusal Toplantısı, TOK2013, 26-28 Eylül 2013, Malatya*
- [7] Philip A. Adewuyi, M.Sc.\* and Emmanuel O. Lawani, B.Eng, "Dynamic Behavior of Brushless DC Motor under the Application of PI, PD, PID, and Fuzzy Logic Controllers" , *Pacific Journal of Science and Technology*. 18(2):5-10, 2017
- [8] Salim, Jyoti Ohri, "FUZZY Based PID Controller for Speed Control of D.C. Motor Using LabVIEW" , *WSEAS TRANSACTIONS on SYSTEMS and CONTROL*, India, 2015

[9] Semih Sezer, Ali Erdem Atalay, “Dynamic modeling and fuzzy logic control of vibrations of a railway vehicle for different track irregularities”, Simulation Modelling Practice and Theory 19 (2011) 1873–1894, Istanbul, Turkey

[10] Vaibhav D. Saundarmal and R. M. Nagarale, “I-P-D TYPE FUZZY CONTROL FOR DC MOTOR”, International Journal of Advances in Engineering & Technology, Nov. 2013.

[11] S. Juraitis, R. Rinkeviciene, J. Kriauciunas, “Fuzzy Controller of Two-mass System” ,ELECTRONICS AND ELECTRICAL ENGINEERING ISSN 1392 – 1215, 2011

[12] Krzysztof Szabat, Teresa Orłowska-Kowalska, “COMPARATIVE ANALYSIS OF DIFFERENT PI/PID CONTROL STRUCTURES FOR TWO-MASS SYSTEM”, Journal of Electrical Engineering.